

IBI GROUP 400-333 Preston Street Ottawa ON K1S 5N4 Canada tel 613 225 1311 fax 613 225 9868 ibigroup.com

Technical Memorandum

To/Attention

Mr. Reinhard Vogel

Date

June 25, 2018

From

Ryan Magladry

Project No

116598 - 5.3.1.

CC

Subject

Turnbull School - Music Room Expansion

Mr. Vogel,

This technical memorandum is prepared in support of the new music room expansion for the Turnbull Private Elementary School located at 1132 Fisher Avenue. IBI Group has been retained by Hobin Architecture Inc. to review the servicing and grading requirements for the 128m2 expansion. This memorandum presents our findings and recommendations regarding the water supply, wastewater disposal, stormwater management and site grading.

Water Supply

The proposed music room expansion consists of a single wash basin for cleaning music instruments. There are no other proposed facilities with significant water demands (bathrooms, showers, etc). The proposed expansion is not sprinklered, but is located within 90m of an existing fire hydrant. This fixture will likely only be used for the last few minutes of each class session when students may clean their instruments, and is not likely to be a constant demand. The addition of this fixture flow will have neglible impacts on the existing water system.

Waste Water Disposal

Based on correspondence with the school principal, the existing school has a student capacity of 410 students and 40 staffer members. The City of Ottawa Sewer Design Guidelines Daily Sewage Flow For Various Establishments, a school <u>without</u> cafeteria or gymnasium with showers has a daily volume of 30L/person/day. Given a population of 450people, the calculated flowrate of the existing school is 0.16L/s.

The Turnbull school property is approximate 1.79Ha. Using the new City of Ottawa Design Guidelines criteria, the school has an infiltration rate of 0.33L/ha/s. The calculated infiltration rate is 0.59L/s.

As previously noted, the proposed music room expansion consists of a single wash basin for cleaning music instruments. The City of Ottawa Sewer Design Guidelines Daily Sewage Flow For Various Establishments – miscellaneous water use estimates for sewage flow computations for wash basins is 375L/day, or 0.004L/s can be used to demonstrate the impacts of the new expansion.

The sum of the existing flows plus the addition of the wash basin is based on City of Ottawa criteria 0.754 L/s + 0.59 L/s + 0.004 L/s.

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The existing sanitary service to the existing school consists of a 200mm diameter sanitary sewer with a designed slope of 1.0%. This pipe has a theoretical full flowing capacity of 34.22 L/s. This is significantly greater than the calculated flows generated by the existing school and the expansion music room.

Stormwater Management

Existing Conditions

The original site grading was designed such that the majority of the existing finished floor is below the finished grade on the north side of the building. As such, the existing foundation was constructed in order to provide adequate exposed concrete (typically referred to as an upstand). In the area of the existing building entrance/exit, there is a small depressed area with a catchbasin. The area captured by Existing CB9 is approximately 214m2 and has a C value of approximately 0.65 (25% grass and 75% asphalt), and was designed to be unrestricted. Refer to the Site Services and Grading drawing prepared by Erion Associates dated December 2002, attached in **Appendix A.**

The pre-expansion unrestricted flow rate to CB9 can be calculated as follows.

Unrestricted Flow to CB9 (Prior to Expansion)

Tc= 10minutes

A= 0.0214ha

 C_{avg} =0.65 x 1.25 = 0.81

I_{100year}=178.6 mm/hr

Qunrest= 2.78 x C x I x A

=2.78 x 0.81 x 178.6 x 0.0214Ha

=8.60 L/s

The remaining areas adjacent to the existing building sheet drained over the existing asphalt pathway and grassed field, and into existing CB1. CB1 is upstream and in-line with CB2. CB2 was designed to contain an inlet control device which restricts flow to the downstream storm sewer network with a custom sized orifice at 144mm diameter. A 144mm orifice with a head 1.25m results in an existing restricted flow rate of **52** I/s.

Proposed Stormwater Management Plan

The proposed expansion will consist of a waterproof flat roof with gentle sloping to provide positive drainage to a single scupper location. The scupper will drain onto a 1.8m x 1.8m hard surface pad to diffuse the roof discharge. The stormwater will sheet drain away from the building onto the recreational use field, before ultimately being captured in existing CB1.

The change in AC tributary to existing CB1 can be summarized as follows:

Removal of area from CB1:

Grass Area (occupied by new roof area) =0.0030Ha @ C=0.25

Paved Area (occupied by new roof area) =0.0038Ha @ C=0.90

Paved Area (new depressed entrance area) =0.0039Ha @ C=0.90

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Total area removed =0.0107Ha

Total Average C =0.72

Total AC removed =0.0077

Addition of area to CB1:

 Roof Area
 =0.0128Ha @ C=0.90

 Grass Area
 =0.0043Ha @ C=0.25

 Total area added
 =0.0171Ha

 Total Average C
 =0.74

 Total AC added
 =0.0126

The AC of the added area to CB1 is greater than the AC of the removed area. Therefore, the flows tributary to CB1 after the expansion will be slightly more than the existing condition. The increase in 100 year flow can be calculated as follows:

100 Year Flow Increase to CB1

Tc= 10minutes

ACincrease = 0.0126-0.0077=0.0049

Runoff Increase Factor = 1.25

 $I_{100year} = 178.6 \text{ mm/hr}$

Q_{unrest} = 2.78 x AC x 1.25 x I

=2.78 x 0.0049 x 1.25 x 178.6

=3.04 L/s

The existing Inlet Control Device (ICD) in CB2 can remain to ensure no negative impacts on downstream storm sewers. The relatively minor increase in total flow to the overall catchment will be retained upstream of the ICD within underground structures, pipes and on surface ponding. Once all stormwater storage facilities are have reached capacity, the flows will spill into the adjacent drainage ditch which also serves as the outlet for the site.

Unrestricted Flow to Storm Sewer at new depressed entrance CB101

The new depressed entrance should maintain unrestricted flow into the existing storm sewer. The flows for the depressed area can be calculated as follows.

Tc= 10minutes

A= 0.0039ha

 C_{avg} =0.90 x 1.25 = 1.0

I_{100year}=178.6 mm/hr

Qunrest = $2.78 \times C \times I \times A$ = $2.78 \times 1.0 \times 178.6 \times 0.0039$ Ha

=1.93 L/s

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The unrestricted flow to the storm sewer is less than the pre-development unrestricted flow to CB9.

New restricted flow to Storm Sewer at new CB100

The area to the east of the proposed expansion, which was previously part of the unrestricted depressed area, is intended to be filled in to closely match the existing surrounding grades. As a result of the updated grading, a low point is required, and thus a new catch basin (CB100). The residual capacity into the storm sewer network is calculated as follows:

Existing Conditions Unrestricted Flow to Storm sewer = 8.60 l/s

Less unrestricted flow to storm sewer (post expansion) = - 1.93 l/s

Residual capacity to meet SWM Targets at new CB100 = 6.67 l/s

Therefore, an ICD will be proposed to restrict flows to the storm sewer. The ICD proposed will consist of an IPEX LMF ICD set to restrict flows to the storm sewer to 6.0 l/s.

The sum of all restricted and unrestricted inlets impacted by the building expansion ($52 \text{ l/s} @ CB2 + 1.93 \text{ l/s} @ unrestricted entrance + 6.0 \text{ l/s} @ new CB100 = <math>\underline{59.93 \text{ l/s}}$) is less than the sum of the restricted and unrestricted inlets prior to the expansion (52 l/s @ CB2 + 8.60 l/s @ old unrestricted entrance = $\underline{60.60 \text{ l/s}}$). The above demonstrates that the total peak flow rate to the sewer network post-expansion is less than pre-expansion. Therefore no net negative impact on the downstream storm sewer system is anticipated.

Site Grading

The grading for the new building expansion will consist of re-shaping the existing grade around the perimeter of the proposed building. As previously noted, the proposed grading will consist of a depressed area serviced by a ramp to the relocated existing building entrance and raising the grade along the eastern façade of the new building to eliminate the previously depressed entrance.

Conclusion

The Turnbull School music room expansion can be serviced by existing infrastructure. Existing water distribution, waste water disposal and stormwater management systems are all adequately sized to accommodate the building expansion.

Ryan Magladry, C.E.**7**.

Demetrius Yannoulopoulos, P. Eng.



